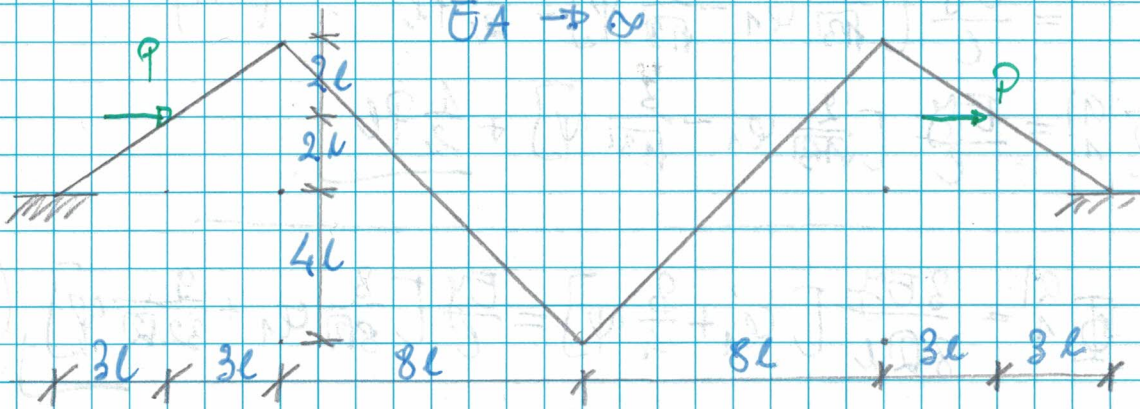


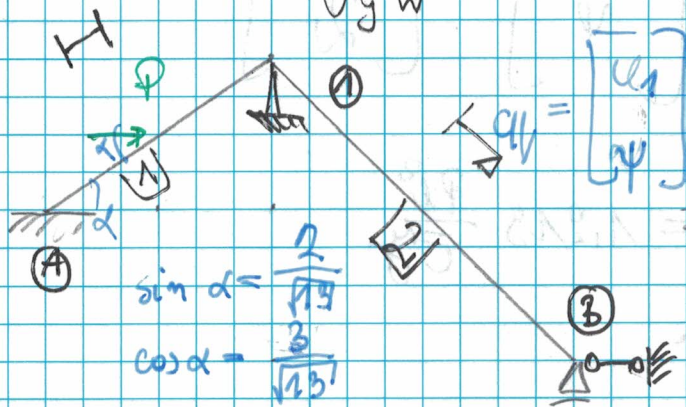
$EY = \text{const.}$

$EA \rightarrow \infty$



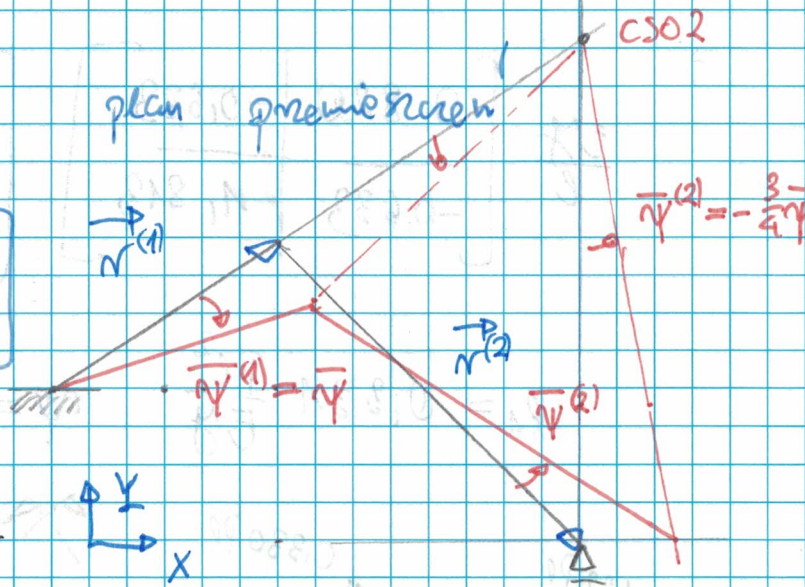
Schemat połączenia

UGW



$\sin \alpha = \frac{2}{\sqrt{13}}$
 $\cos \alpha = \frac{3}{\sqrt{13}}$

plan prężeń



$\vec{r}^A = [6L, 4L]$

$\vec{r}^B = [8L, -8L]$

met. analityczna

$0 = 0 - 6L \psi^{(1)} - 8L \psi^{(2)}$

$\psi^{(1)} = \psi$

$\psi^{(2)} = -\frac{3}{4} \psi$

n. r. MP

$\Phi_A^{(1)} + \Phi_B^{(2)} = 0 \quad (1)$

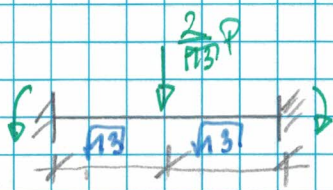
$(\Phi_A^{(1)} + \Phi_B^{(1)}) \psi + \Phi_B^{(2)} (-\frac{3}{4} \psi) + P \cdot \psi \cdot 2L = 0 \quad \psi = -1$

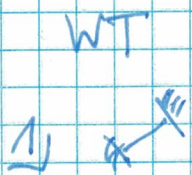
$-(\Phi_A^{(1)} + \Phi_B^{(1)}) + \frac{3}{4} \Phi_B^{(2)} - 2PL = 0$

$\Phi_A^{(1)} = -\frac{1}{8} \frac{2}{\sqrt{13}} P \cdot 2\sqrt{13} L = -\frac{1}{2} PL$

$\Phi_B^{(1)} = \frac{1}{2} PL$

Momenty wyidealne

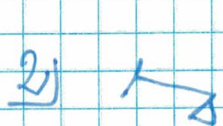




$$\Phi_{-4}^{(1)} = \frac{3EY}{2\sqrt{3}l} [\psi_1 - 3\psi] - \frac{1}{2}Pl =$$

$$= \frac{EY}{l} \left[\frac{1}{\sqrt{3}} \psi_1 - \frac{3}{\sqrt{3}} \psi \right] - \frac{1}{2}Pl \quad (-1)$$

$$\Phi_{+1}^{(1)} = \frac{EY}{l} \left[\frac{2}{\sqrt{3}} \psi_1 - \frac{3}{\sqrt{3}} \psi \right] + \frac{1}{2}Pl$$

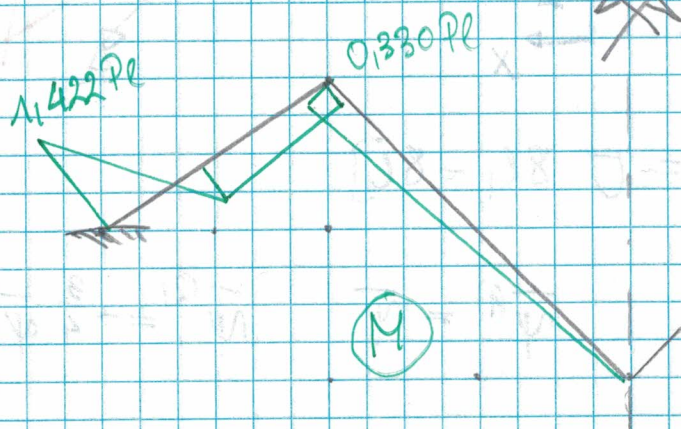


$$\Phi_{+1}^{(2)} = \frac{3EY}{8Ql} \left[\psi_1 + \frac{9}{4}\psi \right] = \frac{EY}{l} \left[\frac{3}{8Q} \psi_1 + \frac{9}{32Q} \psi \right] \quad \left(\frac{3}{2} \right)$$

$$\frac{EY}{l} \begin{bmatrix} 0,820 & -0,633 \\ -0,633 & 1,813 \end{bmatrix} \begin{bmatrix} \psi_1 \\ \psi \end{bmatrix} = \begin{bmatrix} -0,5 \\ 2 \end{bmatrix} Pl$$

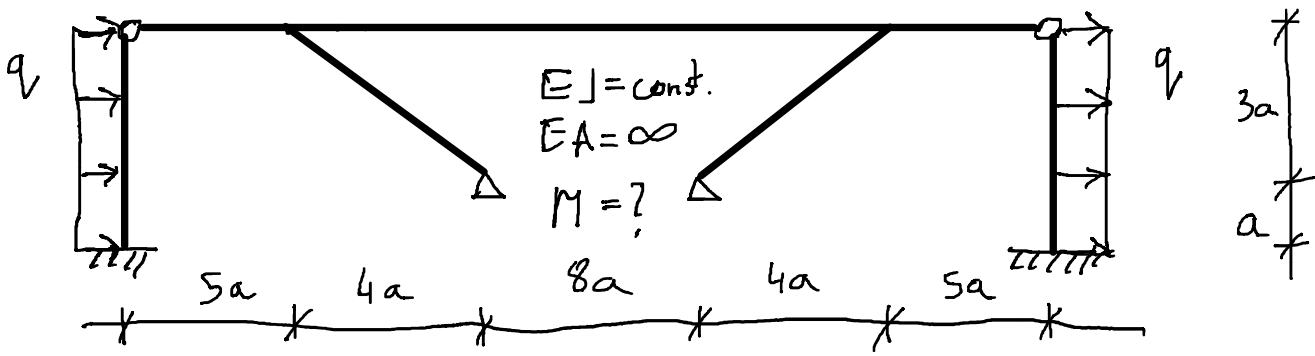
$$\psi_1 = 0,331 \frac{Pl^2}{EY}$$

$$\psi = 1,219 \frac{Pl^2}{EY}$$

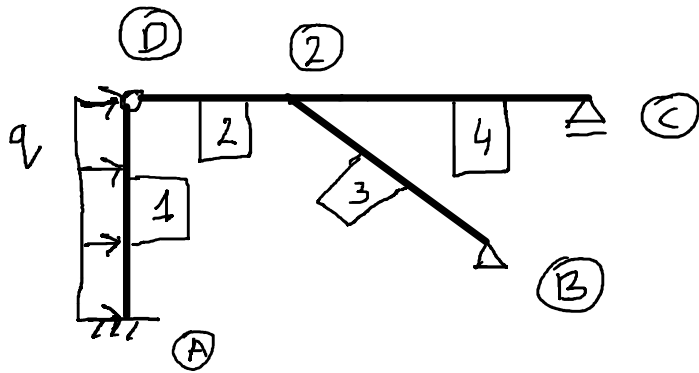


K2.1

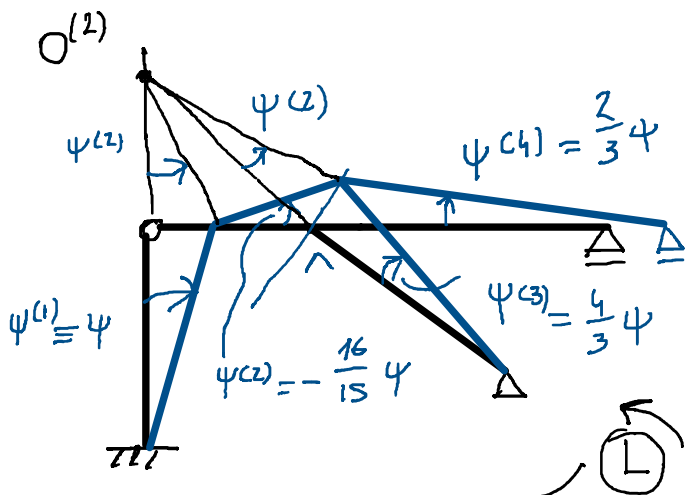
9 I 2025



SCHEMAT POŁÓWKOWY



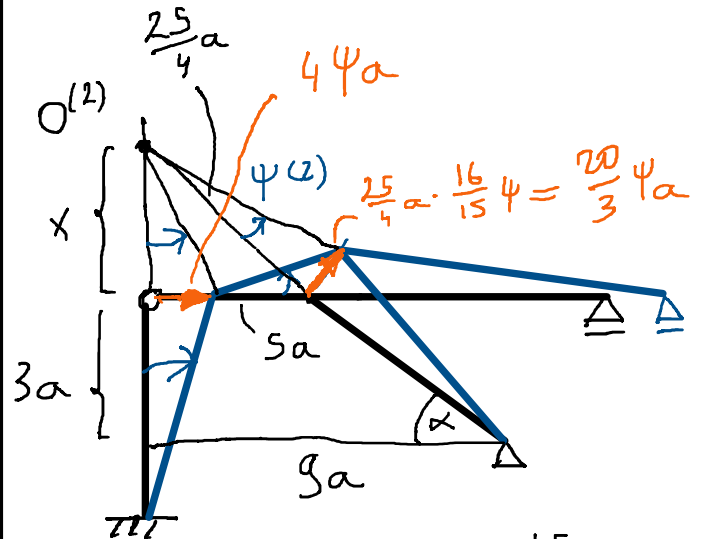
PLAN PRZEMIESZCZEŃ



$$\psi^{(2)} = \frac{4\psi a}{\frac{15}{4}a} = -\frac{16}{15}\psi$$

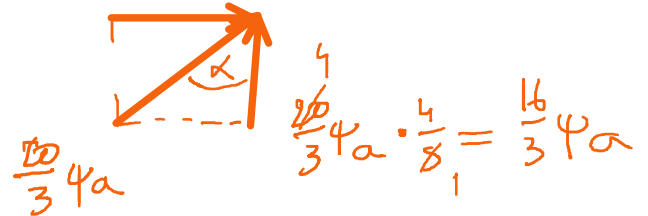
$$\psi^{(3)} = \frac{\frac{20}{3}\psi a}{5a} = \frac{4}{3}\psi$$

— ciężary prostów



$$\frac{x}{5a} = \frac{x+3a}{9a} \Rightarrow x = \frac{15}{4}a$$

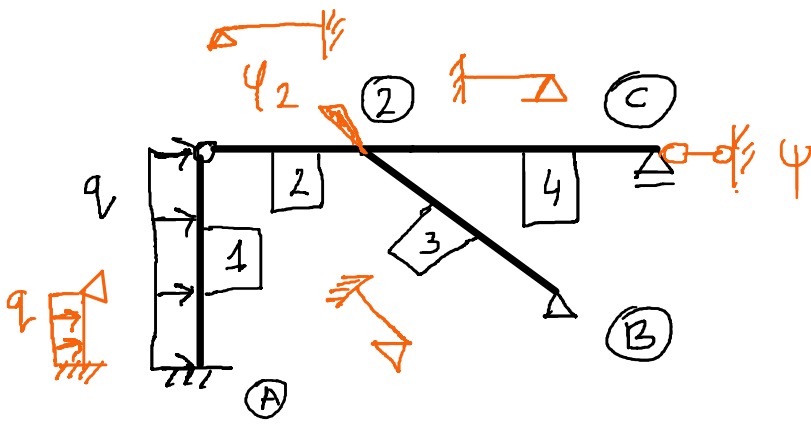
$$\frac{20}{3}\psi a \cdot \frac{3}{5} = 4\psi a$$



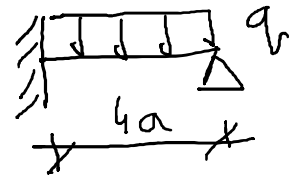
$$\psi^{(4)} = \frac{16\psi a}{3 \cdot 8a} = \frac{2}{3}\psi$$

$$\psi^{(1)} \equiv \psi$$

UGW



$$q = \begin{bmatrix} \psi_2 \\ \psi \end{bmatrix}$$



$$\phi_A^{(1)} = - \frac{q(4a)^2}{8} = -2qa^2$$

RAMP

$$1) \phi_2^{(2)} + \phi_2^{(3)} + \phi_2^{(4)} = 0$$

$$2) \phi_A^{(1)} \cdot \bar{\psi}^{(1)} + \phi_2^{(2)} \cdot \bar{\psi}^{(2)} + \phi_2^{(3)} \cdot \bar{\psi}^{(3)} + \phi_2^{(4)} \cdot \bar{\psi}^{(4)} + \bar{L}_{0B3C}^{0B3C}_{ZEW} = 0$$

$$\bar{L}_{0B3C}^{0B3C}_{ZEW} = q \cdot 4a \cdot 2\bar{\psi}a = 8\bar{\psi}qa^2$$

WZORY TRANSFORM.

$$\phi_A^{(1)} = \frac{3EJ}{4a} [-\psi^{(1)}] - 2qa^2$$

$$\phi_2^{(2)} = \frac{3EJ}{5a} [\psi_2 - \psi^{(2)}]$$

$$\phi_2^{(3)} = \frac{3EJ}{5a} [\psi_2 - \psi^{(3)}]$$

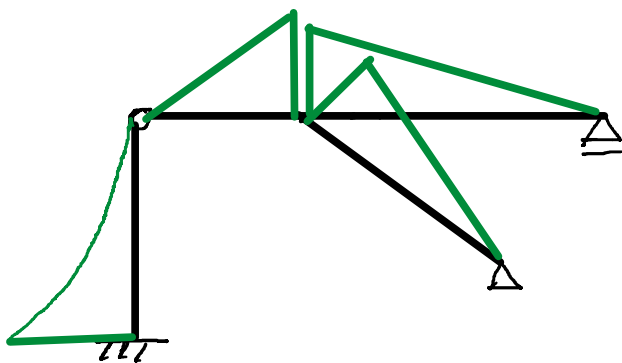
$$\phi_2^{(4)} = \frac{3EJ}{8a} [\psi_2 - \psi^{(4)}]$$

po podstawieniu w 2) $\bar{\psi} = -1$, w po podstawieniu reszty wielkości do równań, otrzymamy

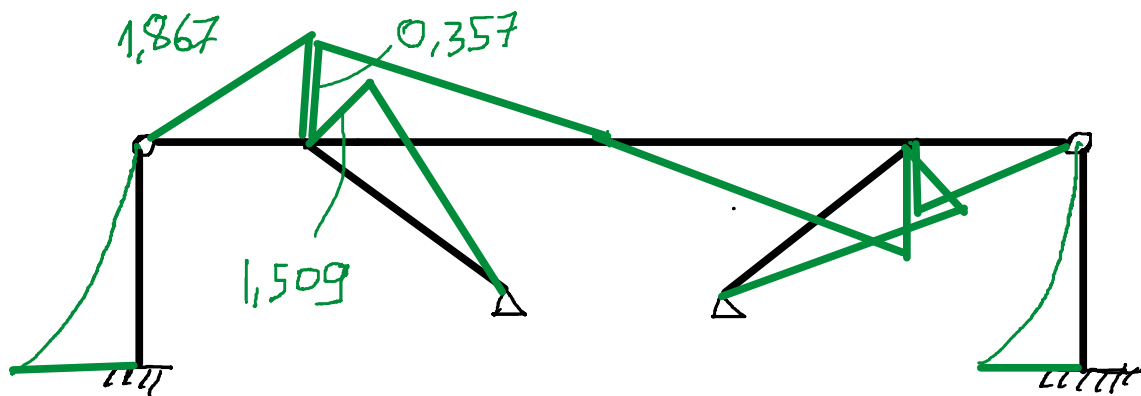


$$\frac{EJ}{a} \begin{bmatrix} 1,575 & -0,41 \\ -0,41 & 2,666 \end{bmatrix} \begin{bmatrix} \varphi_2 \\ \psi \end{bmatrix} = qa^2 \begin{bmatrix} 0 \\ 6 \end{bmatrix}$$

$$\Rightarrow \begin{cases} \varphi_2 = 0,610 \frac{qa^3}{EJ} \\ \psi = 2,344 \frac{qa^3}{EJ} \end{cases}$$



$$M [qa^2]$$



$$3,758$$

$$\Sigma M_{(2)} \cong 0$$