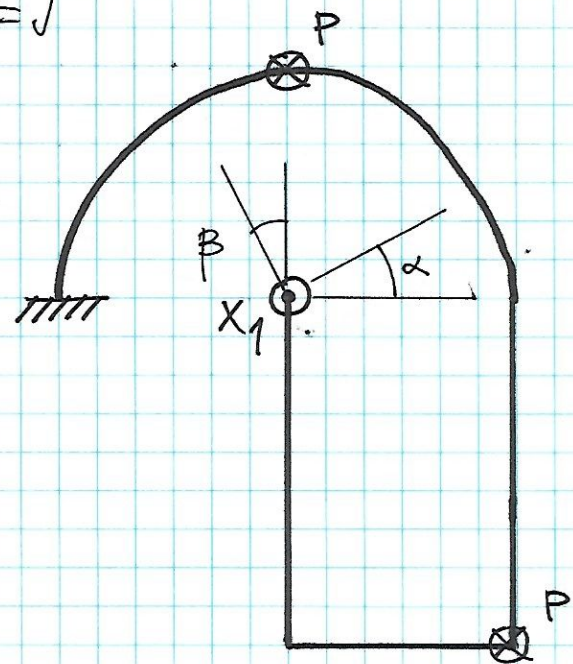
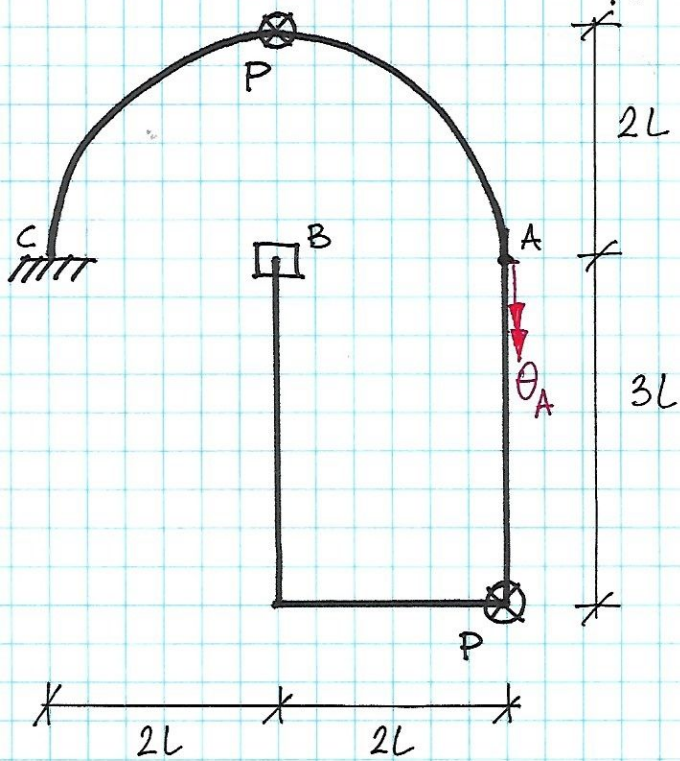


Oblicz kąt obrotu  $\theta_A$ .

$GJ_s = EJ$

Schemat zastępczy

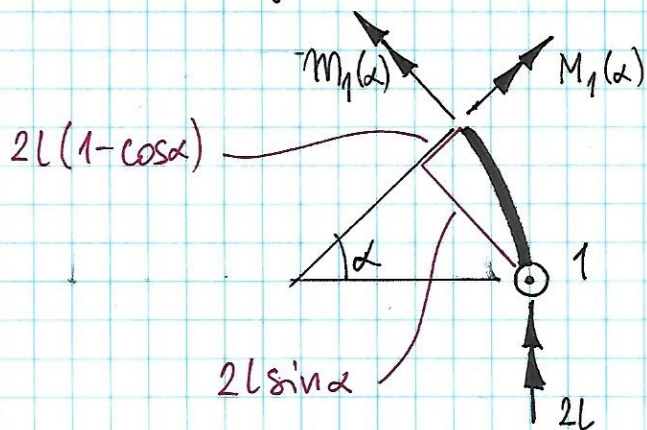
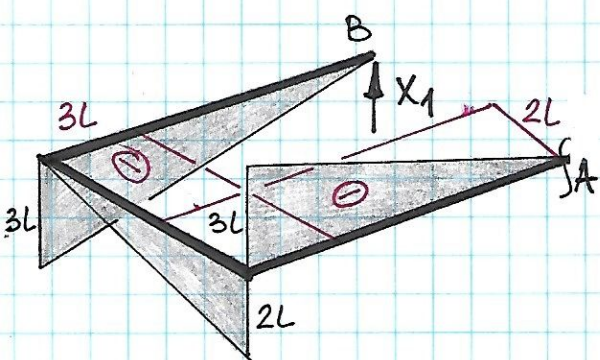


$X_1 = 1$

pręty proste (część A-B)

tuk katowy (część A-C)

$M_1$   $m_1$



$$M_1(\alpha) - 1 \cdot 2L \sin \alpha + 2L \cdot \sin \alpha = 0$$

$$M_1(\alpha) = 0$$

$$M_1(\alpha) + 1 \cdot 2L(1 - \cos \alpha) + 2L \cdot \cos \alpha = 0$$

$$M_1(\alpha) = -2L$$

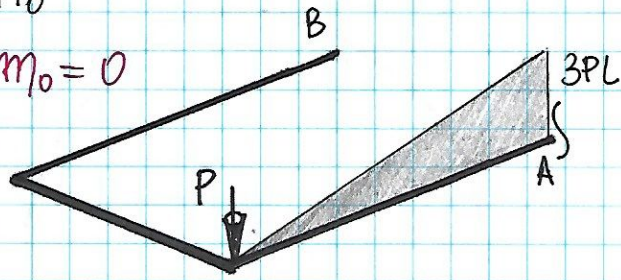
$$\delta_{11} = \frac{1}{EJ} [20,67 L^3] + \frac{1}{GJ_s} [55,13 L^3] = 75,80 \frac{L^3}{EJ}$$

Stan "0"

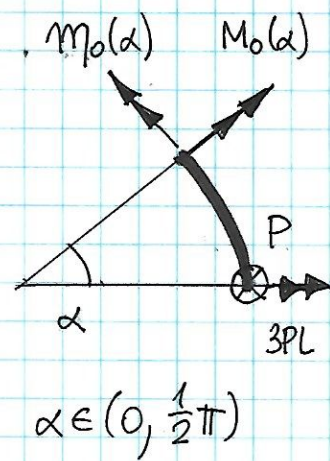
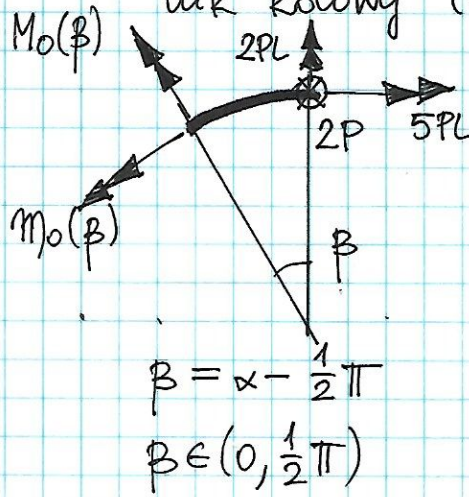
pręty proste (część A-B)

$M_0$

$m_0 = 0$



Tuk kotowy (część A-C)



$\alpha$ :  $M_0(\alpha) + P \cdot 2L \sin \alpha + 3PL \cos \alpha = 0 \rightarrow M_0(\alpha) = -2PL \sin \alpha - 3PL \cos \alpha$

$m_0(\alpha) - P \cdot 2L(1 - \cos \alpha) - 3PL \sin \alpha = 0 \rightarrow m_0(\alpha) = 2PL + 3PL \sin \alpha - 2PL \cos \alpha$

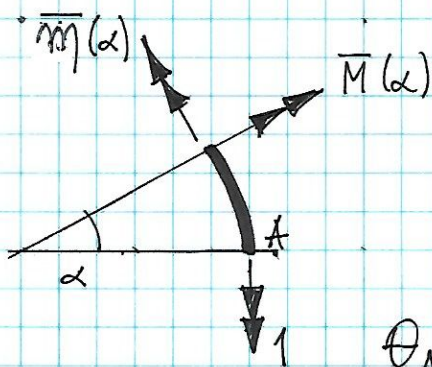
$\beta$ :  $M_0(\beta) + 2P \cdot 2L \sin \beta + 2PL \cos \beta - 5PL \sin \beta = 0 \rightarrow M_0(\beta) = PL \sin \beta - 2PL \cos \beta$

$m_0(\beta) - 2P \cdot 2L(1 - \cos \beta) - 2PL \sin \beta - 5PL \cos \beta = 0 \rightarrow m_0(\beta) = 4PL + 2PL \sin \beta + PL \cos \beta$

$\delta_{10} = \frac{1}{EJ} [4,5 PL^3] + \frac{1}{GJs} [-53,70 PL^3] = -49,20 \frac{PL^3}{EJ}$

$X_1 = 0,65 P$

Obciążenie jednostkowe "w kierunku"  $\theta_A$  w schemacie statycznie wyznaczalnym nie wywołuje sił wewnętrznych w prętach prostych.



$\bar{M}(\alpha) - 1 \cdot \sin \alpha = 0 \rightarrow \bar{M}(\alpha) = \sin \alpha$

$\bar{m}(\alpha) - 1 \cdot \cos \alpha = 0 \rightarrow \bar{m}(\alpha) = \cos \alpha$

$\bar{M}(\beta) = \bar{M}(\alpha - \frac{1}{2}\pi)$ ,  $\bar{m}(\beta) = \bar{m}(\alpha - \frac{1}{2}\pi)$

$\theta_A = \frac{1}{EJ} \int_{A-C} M \bar{M} ds + \frac{1}{GJs} \int_{A-C} m \bar{m} ds =$

$= \frac{1}{EJ} \int_{A-C} (M_1 X_1 + M_0) \bar{M} ds + \frac{1}{GJs} \int_{A-C} (m_1 X_1 + m_0) \bar{m} ds$

$= -16,57 \frac{PL^3}{EJ}$

Opracował Szymon Spodzieja