

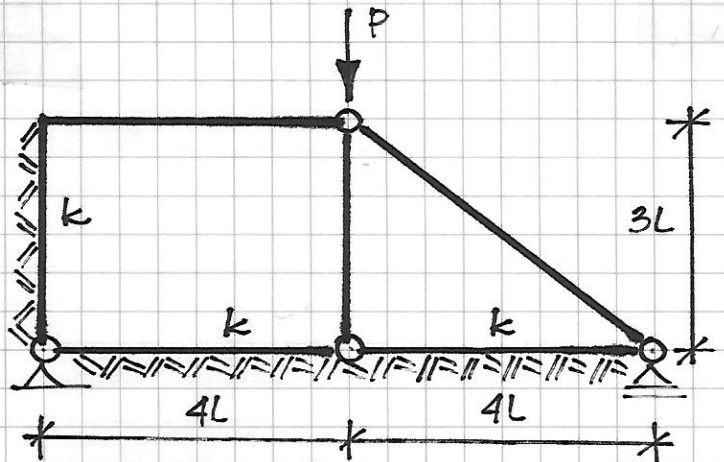
Egzamin z Mechaniki Konstrukcji (MK3 IPB), 20.06.2018
studia stacjonarne

NAZWISKO, Imię				
rok akademicki zaliczenia ćwiczeń	nr albumu	grupa (IPB / BZ)	tryb studiów (ST / NST)	
ocena zadania 1	ocena zadania 2	ocena zadania 3	ocena egzaminu	ocena łączna

Zadanie 1.

$EJ = const., \quad k = 0,0064 \frac{EJ}{l^4}$

Oblicz siły podłużne w prętach pionowych ramy z rys. 1.



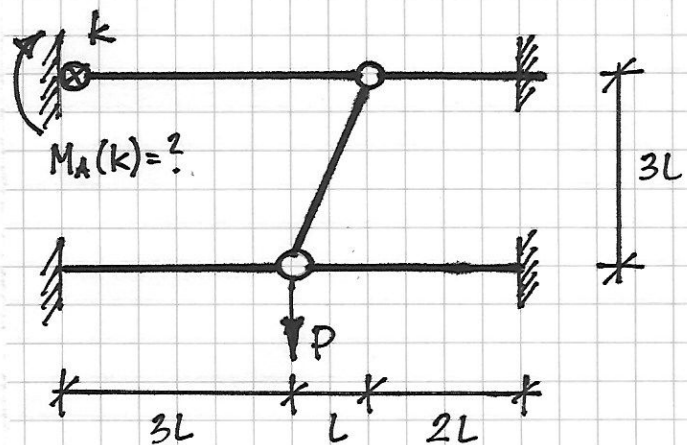
rys. 1.

Zadanie 2.

$EJ = const.$

Oblicz wartość $M_A(k)$ w ramie z rys. 2

dla $k = \frac{EJ}{l}, k = 3 \frac{EJ}{l}, k = 10 \frac{EJ}{l}, k = +\infty$



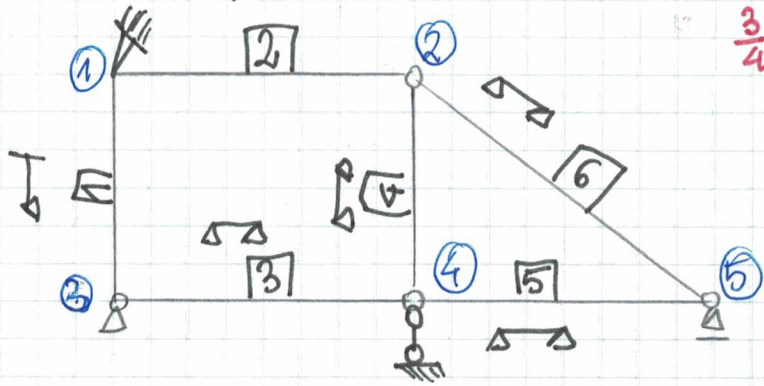
rys. 2.

Zadanie 3.

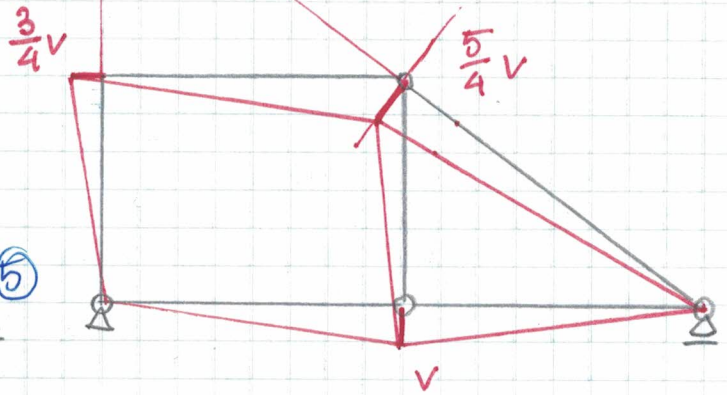
Wyprowadź wzór transformacyjny określający moment przywęzłowy w pręcie podpartym według schematu Πa (patrz na odwrocie) metodą kondensacji statycznej ugięcia prawego węzła w pręcie podpartym według schematu Ia.

ZADANIE 1 NST II IPB 20VI 2018

UGW $q = \left[\varphi \quad \frac{v}{l} \right]^T$



Plan przesunięć



Prełt	$l^{(n)}$	$\alpha^{(n)}$	$*w$	w^*
1	$3l$	$0,6$	0	$-\frac{3}{4}v$
2	$4l$	0	0	v
3	$4l$	$0,8$	0	v
4	$3l$	0	0	$-\frac{3}{4}v$
5	$4l$	$0,8$	v	0
6	$5l$	0	$\frac{5}{4}v$	0

n.r. MP

$$\Phi_1^{(1)} + \Phi_1^{(2)} = 0 \quad (1)$$

$$-(W_4^{(3)} v + W_4^{(5)} v + W_1^{(1)} (-\frac{3}{4}v) + W_2^{(2)} v) + P v = 0 \quad (2)$$

Wzory transformacyjne

$$\Phi_1^{(1)} = \frac{EY}{3l} \left[\alpha'(0,6) \varphi - \theta'(0,6) \frac{(-\frac{3}{4}v)}{3l} \right] = \frac{EY}{l} [1,003 \varphi + 0,254 \frac{v}{l}]$$

$$W_1^{(1)} = -\frac{EY}{(3l)^2} \left[\theta'(0,6) \varphi - \gamma'(0,6) (-\frac{3}{4}v) \cdot \frac{1}{3l} \right] = \frac{EY}{l^2} [-0,338 \varphi - 0,090 \frac{v}{l}]$$

$$\Phi_1^{(2)} = \frac{EY}{4l} \left[\alpha'(0) \varphi - \delta'(0) \frac{v}{4l} \right] = \frac{EY}{l} [0,75 \varphi - 0,188 \frac{v}{l}]$$

$$W_2^{(2)} = -\frac{EY}{(4l)^2} \left[\delta'(0) \varphi - \alpha'(0) \frac{v}{4l} \right] = \frac{EY}{l^2} [-0,188 \varphi + 0,047 \frac{v}{l}]$$

$$W_4^{(3)} = -\frac{EY}{(4l)^2} \left[-\gamma'''(0,8) \frac{v}{4l} \right] = \frac{EY}{l^2} [0,008 \frac{v}{l}]$$

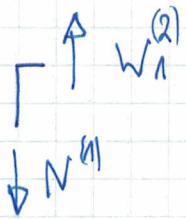
$$W_4^{(5)} = \frac{EY}{(4l)^2} \left[\gamma'''(0,8) \frac{v}{4l} \right] = \frac{EY}{l^2} [0,008 \frac{v}{l}]$$

$$\frac{Eg}{l} \begin{bmatrix} 1,753 & 0,066 \\ 0,066 & 0,131 \end{bmatrix} \begin{bmatrix} \varphi \\ \frac{v}{l} \end{bmatrix} = \begin{bmatrix} 0 \\ 1 \end{bmatrix} Pl$$

$$\varphi = -0,293 \frac{Pl^2}{Eg}$$

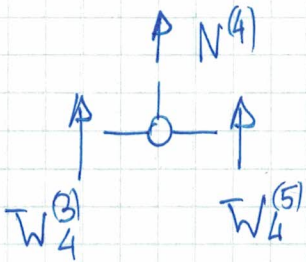
$$v = 7,781 \frac{Pl^3}{Eg}$$

Wegzeit ①



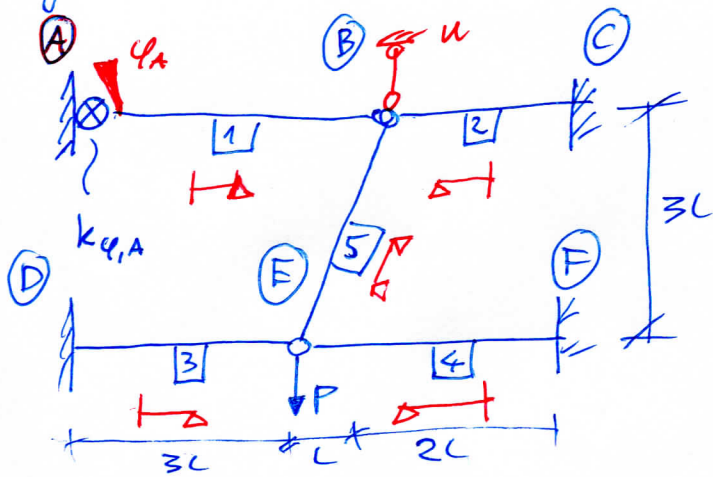
$$N^{(1)} = W_1^{(2)} = -0,420 P$$

Wegzeit ④



$$N^{(4)} = - (W_4^{(3)} + W_4^{(5)}) = -0,125 P$$

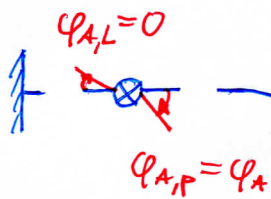
Examin MK IPB stac. 20.06.18r, Zadanie 2



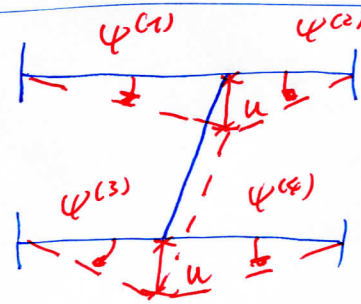
$$k_{\varphi, A} = \tau \frac{EJ}{L}$$

$$q = \begin{bmatrix} \varphi_A \\ u/L \end{bmatrix}$$

Kinematyka:



$$\Delta \varphi_A = \varphi_{A,P} - \varphi_{A,L} = \varphi_A - 0 = \varphi_A$$



$$\begin{aligned} \varphi^{(1)} &= \frac{u}{4L} \\ \varphi^{(2)} &= -\frac{u}{2L} \\ \varphi^{(3)} &= \frac{u}{3L} \\ \varphi^{(4)} &= -\frac{u}{3L} \\ \varphi^{(5)} &= 0 \end{aligned}$$

RRMP:

1) $\Phi_A^{(1)} + Q_{\varphi, A} = 0$

2) RPW:

$$\Phi_A^{(1)} \cdot \left(\frac{\bar{u}}{4L}\right) + \Phi_C^{(2)} \cdot \left(-\frac{\bar{u}}{2L}\right) + \Phi_D^{(3)} \cdot \left(\frac{\bar{u}}{3L}\right) + \Phi_F^{(4)} \cdot \left(-\frac{\bar{u}}{3L}\right) + P \cdot \bar{u} = 0 \quad | \cdot (-1); \bar{u} = L$$

Wzrosty transformacyjne:

$$\begin{aligned} \Phi_A^{(1)} &= \frac{EJ}{(4L)} \left[3\varphi_A - 3 \cdot \left(\frac{u}{4L}\right) \right]; \quad \Phi_C^{(2)} = \frac{EJ}{(2L)} \left[-3 \cdot \left(-\frac{u}{2L}\right) \right]; \\ \Phi_D^{(3)} &= \frac{EJ}{(3L)} \left[-3 \cdot \left(\frac{u}{3L}\right) \right]; \quad \Phi_F^{(4)} = \frac{EJ}{(3L)} \left[-3 \cdot \left(-\frac{u}{3L}\right) \right] \end{aligned}$$

Związek konstytatywny węzła podanego:

$$Q_{\varphi, A} = k_{\varphi, A} \cdot \Delta \varphi_A$$

$$Q_{\varphi, A} = \frac{EJ}{L} [\tau \cdot \varphi_A]$$

$$\frac{EJ}{L} \begin{bmatrix} \frac{3}{4} + \tau & -\frac{3}{16} \\ -\frac{3}{16} & \frac{341}{576} \end{bmatrix} \begin{bmatrix} \varphi_A \\ u/L \end{bmatrix} = \begin{bmatrix} 0 \\ PL \end{bmatrix} \Rightarrow$$

$$\varphi_A = \varphi_A(\tau) = \frac{108}{258 + 341\tau} \frac{PL^2}{EJ}$$

$$u = u(\tau) = \dots$$



$$\Rightarrow M_A = -Q_{\varphi, A} = -\frac{EJ}{L} [\tau \cdot \varphi_A] = -\frac{108\tau}{258 + 341\tau} PL =: M_A(\tau)$$

$$M_A(\infty) = \Phi_A^{(1)} = -0.291 \frac{PL}{PL}$$

$$M_A(1) = -0.172 PL$$

$$M_A(3) = -0.236 PL$$

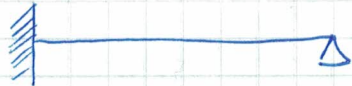
$$M_A(10) = -0.242 PL$$

$$M_A(\infty) = \lim_{\tau \rightarrow \infty} M_A(\tau) = -\frac{108}{341} PL = -0.291 PL$$

Albo: $k_{\varphi, A} = \infty \Rightarrow$ *definiği* $\Delta \varphi_A = 0 \Rightarrow \varphi_A = 0 \Rightarrow$

$$\Rightarrow -\frac{3}{16} \cdot 0 + \frac{341}{576} \frac{u}{L} = PL \Rightarrow u = \frac{576}{341} PL \Rightarrow \Phi_A^{(1)} = \frac{EJ}{(4L)} \left[0 - 3 \cdot \left(\frac{u}{4L}\right) \right] = -0.291 PL$$

Schemat $\bar{I}a$

 Dobieramy w^* tak, aby $w^* = 0$

$$w^* = -\frac{EY}{l^2} \left[\delta'(x) * \varphi + \varepsilon'(x) \frac{*w}{l} - \alpha'(x) \frac{*w}{l} \right] = 0$$

$$\Rightarrow w^* = \frac{l}{\alpha'(x)} \left[\delta'(x) * \varphi + \varepsilon'(x) \frac{*w}{l} \right]$$

Podstawiamy do wzoru na $*\Phi$

$$*\Phi = \frac{EY}{l} \left[\alpha'(x) * \varphi + \theta'(x) \frac{*w}{l} - \frac{\delta'(x)}{\alpha'(x)} \left(\delta'(x) * \varphi + \varepsilon'(x) \frac{*w}{l} \right) \right] =$$

$$= \frac{EY}{l} \left[\left(\alpha'(x) - \frac{(\delta'(x))^2}{\alpha'(x)} \right) * \varphi + \left(\theta'(x) - \frac{\delta'(x) \varepsilon'(x)}{\alpha'(x)} \right) \frac{*w}{l} \right] =$$

$$= \frac{EY}{l} \left[\alpha''(x) * \varphi + \theta''(x) \frac{*w}{l} \right]$$

Otrzymujemy wzór na $*\Phi$ pręta podpartego wg schematu $\bar{II}a$.

